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INCREASING ELECTRICITY SELF-CONSUMPTION IN RESIDENTIAL BUILDINGS BY ELECTRICITY-TO-HEAT CONVERSION AND STORAGE

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The current paper addresses energy storage issues in residential buildings with the objective of increasing direct consumption. The building, connected to an utility grid, is supplied by a micro wind turbine and PV panels. The utility grid itself acts as an energy buffer. Only nonshiftable loads (white goods, TV etc.) and electric water heating are taken into account. The studied configuration comprises two cascaded heating boilers, one of them preheating boiler. The annual electricity production of the micro wind turbine and PV panels is chosen to cover the hot water demand and nonshiftable loads inside the building with 70/30 ratio in favour of the wind energy. During the experiments, the generation graphs' shaving levels vary between 0 and 100 %, with peak energy diverted into a preheating boiler and the remaining part fed into the main boiler. The proposed solution allows increasing locally consumed energy share, as the energy of stochastic peaks is stored and used on later demand. The locally consumed energy is expressed by the cover factor, its increase possibilities are studied in main text. Calculations are based on 5- minute time series. The applied algorithm follows the amount of heat in the main and preheating boiler, including also incoming and outgoing energies. The cover factor cannot be increased without restrictions. Too high shaving levels bring along problem of removing excess heat from the preheating boiler. The allowed drain loss is taken as 10 % of annual boiler energy balance. The presumed growth of the cover factor at preheating boiler volume of 160 l instead of 80 l is at least 8 % . with the main boiler sized as before.

Keywords: cover factor, demand response, domestic hot water, load shifting, solar energy, wind energy

INTRODUCTION

Amidst all renewable energy sources, the wind and solar ones have the longest historical records with increasing expansion pace during the last decade (Kaldellis and Zafirakis, 2011). The rapid growth of the wind and solar share in the overall energy mix is mainly related to large installations in form of generation parks. As for micro wind and solar power, the growth is encouraged by the EU requirements on net zero-energy buildings (Kaldellis and Zafirakis, 2011). The largely fluctuating and unpredictable power output of wind and solar installations is a common knowledge (Allik and Annuk, 2016; Tabone and Callaway, 2014; Ming et al., 2015). To alleviate the stochastic character of the described primary energy sources, several local demand side management (DSM) approaches are applied. The application of heat pumps is one of the most widespread ones, discussed in the current paper as well (Vanhoudt et al., 2014; Elkinton et al.,

2009). Other peak shaving possibilities of stochastic power generation graphs include batteries (Iqbal, 2004; Rahmoun, et al., 2016; Rosin et al., 2012), pumped hydro storage (Zoss et al., 2015), direct current (DC) loads (Gabbar and Abdelsalam, 2014; Loh et al., 2014), enhanced wind and solar generation forecast (Aguilar et al., 2014) or compressed air storage (Ciocan et al., 2015). In principle, there exist two types of measures to alleviate stochastics of the primary sources, either to store the produced energy partially or fully and reuse it later, or to increase the share of direct demand by applying different methods. Both of them have their disadvantages. The article combines both approaches with additional heating boiler alleviating the stochastics of wind and solar inputs (Allik et al., 2016; Pourmousavi et al., 2014), optionally load shifting can be applied (Hassanzadeh et al., 2017). The additional preheating boiler stores the peaks of the wind and solar generation graphs. During the simulations, both (wind and solar) generation graphs were shaved at different levels between 0 to 100 % of the rated power, where 0 % describes the situation when all the incoming energy is fed into a preheating boiler and at 100 %, there is no peak shaving at all. Both the wind and solar generation graphs are shaved similarly. The study aims studying the possibilities of increasing the supply cover factor in a residential building with two heating boilers installed as energy storage units. Volume of the main boiler remains the same, but one can vary the volume of the preheating boiler and find how does it act upon the cover factor.

MATERIALS AND METHODS

The wind turbine and PV panels are located on a building roof at 58°23'19" N, 26°41'37" E. The network analyzer Janitza UMG 605 (Janitza...,2017) with current transformers Circutor P2 TC5 M70312 provides the data acquisition (Circutor..., 2017). The time series begins with December, 2015 and ends with November, 2016. The production graphs are shaved at the 5 minute averaged actual power levels, whereas the succeeding calculations are based on the corresponding 5 minute sum energy portions.

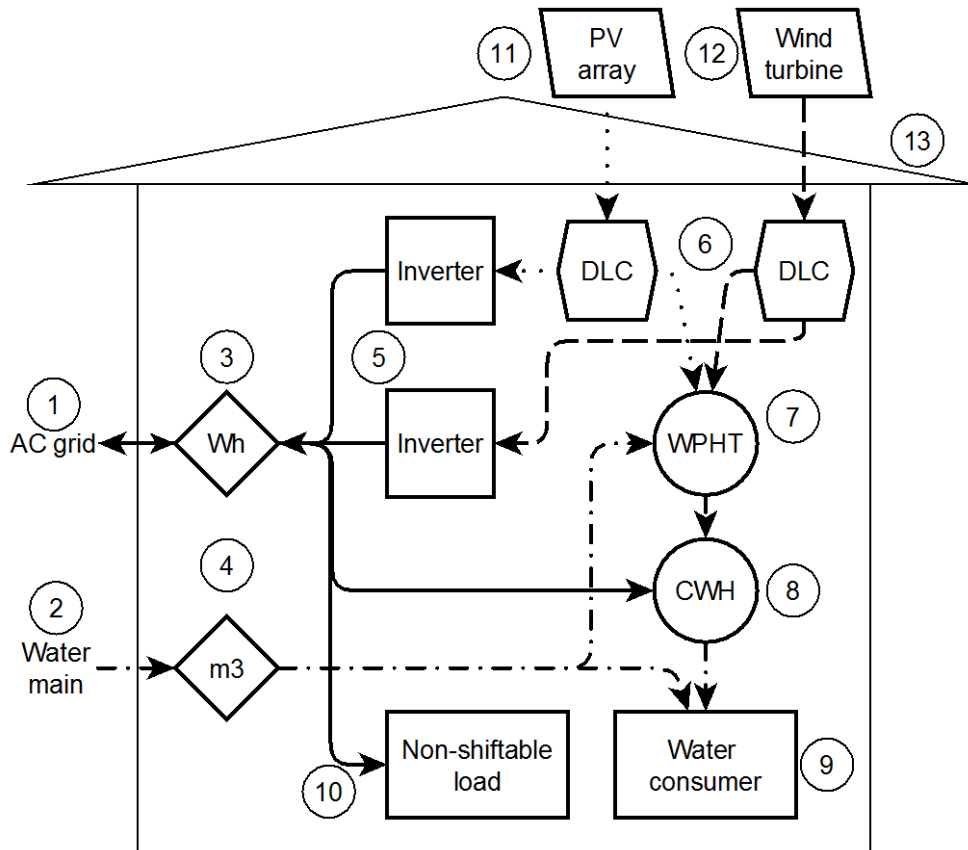


Figure 1. With two boiler equipped energy storage principal solution scheme

Where: Solid line – AC flow, dashed line – variable frequency AC flow, dash-dot line – water flow, dotted line – DC flow, 1 – AC grid, 2 – Water main line, 3 – bidirectional electrical energy meter, 4 – water meter, 5 – inverters for PV array and wind turbine, 6 – dump load controller (DLC), 7 – water pre-heater boiler (WPHT), 8 – conventional water heater (CWH), 9 – Hot and cold water consumer, 10 – non-shiftable loads (HVAC, TV, etc), 11 – PV panels, 12 – Wind turbine, 13 – Near-Zero Energy Building.

Fig. 1 explains a solution with two equally sized boilers, where the first, the preheating one acts as a dump load, absorbing the wind turbine and solar panel shaved peaks. Both the wind turbine and the solar panel have their own heating elements. If the preheating boiler is not capable of absorbing the whole shaved energy from the generating units, an emergency valve opens and drains part of the hot water. The main boiler is meant to accumulate the remaining energy below the generation units' shaving levels and can operate even without the preheating boiler.

The given research discusses a typical household electricity load graph. Two load types are observed: non-shiftable (white goods, TV etc.) and boiler loads. Instead of a single boiler, two equally sized boilers are applied. The household's annual electricity consumption is 3473 kWh, which remains between Estonian (2957 kWh/year) and European Union average values (3601 kWh/year) (World..., 2015). The nonshiftable load counted 1632 kWh/y. The data were initially measured and later brought to scale. The boiler volume selection is based on literature (Allik etc., 2016). Nevertheless, both boilers were chosen with 80 l volume, in the preheating boiler there was a double 2 kW heating element, one to absorb excess power from the wind turbine and the other from the solar panel. The boiler energy capacity was taken 5.4 kWh. The boilers are designed to consume 1840 kWh/y, i.e. 53 % of the total consumption. The boiler load graphs are based on real measurements. For comparison, in Germany the electric boilers consume 13 % and in the United Kingdom, 20 % of a household's electricity (Ferrantelli etc., 2017). The calculations do not include the electricity for room heating purposes. The utility grid acts as an energy buffer absorbing the proficiencies and covering the deficiencies.

The current simulation involves following production devices: horizontal axis, 3.5 kW, passive yaw control permanent magnet generator (Sonkyo..., 2015), with SMA Sunny Boy 3600TL inverter (SMA..., 2017) and 2.5 kW PV array (DelSolar 250 W D6P250B3A) (Yingli..., 2017), orientated towards South with 40° elevation. A 2.75 kW grid tie inverter (SOLIVIA 2.5 EU G3) (SMA..., 2017) is used for DC/AC conversion.

The generation graphs of both the wind turbines and solar panels are based on real measured data and scaled accordingly. The wind turbine is scaled to 5.84 kW and the solar panel set to 1.02 kW. The power ratio is chosen on the basis of a 70/30 annual wind/solar energy mix in favour of the wind energy (Caralis et al., 2011; Annuk et al., 2011; Annuk et al., 2013)). Both generation graphs are shaved on the same level. The wind turbine is located in urban conditions, causing a low capacity factor of $CF=0.06$ and for solar panels, the value is an Estonian average $CF=0.11$.

The cover factors (Allik et al., 2016; Baetens et al., 2012) express both locally produced and directly consumed power shares:

$$Y_S = \frac{\int_{t_0}^{t_1} P_D dt + \int_{t_1}^{t_2} P_S dt}{\int_{t_0}^{t_2} P_S dt} \quad Y_D = \frac{\int_{t_0}^{t_1} P_D dt + \int_{t_1}^{t_2} P_S dt}{\int_{t_0}^{t_2} P_D dt} \quad (1)$$

where P_S is the local power supply and P_D the local power demand. The time when $P_D(t) \leq P_S(t)$ is denoted as $t_0...t_1$, and $t_1...t_2$ is the time when $P_D(t) > P_S(t)$. The supply cover factor is a measure for the self-consumption of locally produced renewable energy (Vanhoudt et al., 2014) . Similarly, the demand cover factor is defined as 'the ratio to which the energy demand is covered by the local supply' and indicates the 'self-generation' (Vanhoudt et al., 2014).

According to the prior work (Annuk et al., 2017), the cover factor can be increased under given circumstances up to $Y_S=Y_D=0.6$ in case when generation graphs are shaved at 25 % level. Although higher cover factor values are achievable, the limiting factor is an increased energy drain loss to avoid the overheating hazard.

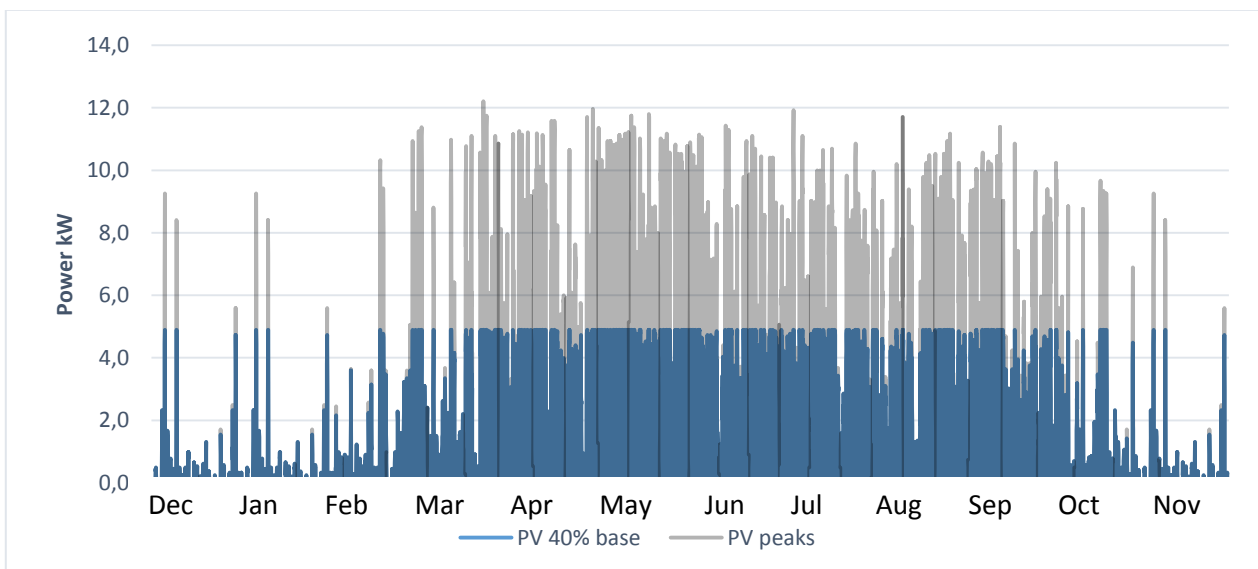


Figure 2. Sample of annual hour-based generation graphs with 40 % shaving level for PV base and peak generation

Fig. 2 exhibits annual hour-based PV generation graphs, showing both the base generation shaved at 40 % level and the shaved peaks. If add here wind turbine production graph, when they are balancing together some extent. In summer time is excess PV electricity, but wind energy production is little bit less intensive in this time. The drain losses, caused by excess overheated water diverted into the drain, are assumed to be equal to the heat dissipation into the surrounding environment, i.e. 10 % (Pournousavi et al., 2014) of the boiler's annual energy balance. The exact energy capacity calculated from the boiler volume is 5.05 kWh, however 5.4 kWh has been taken as the base value. While varying the preheating boiler volume at constant main boiler energy capacity from initial 5.4 kWh to 2.5-fold value the cover factor is assumed to change. Upsizing the main boiler would bring along additional losses into the surrounding ambient, as the heat exchange surface grows as well. The main boiler temperature must

remain constant, additional energy is taken from the utility grid when needed. Upsizing the preheating boiler does not result in more losses, as the passing energy remains the same. The calculations are based on the MatLab software suite.

RESULTS AND DISCUSSION

The section provides an analysis overview of the conception and solution proposed in the previous section. Fig. 3 brings into evidence the impact of different preheating boiler volumes on the cover factor, which rises up to 0.7.

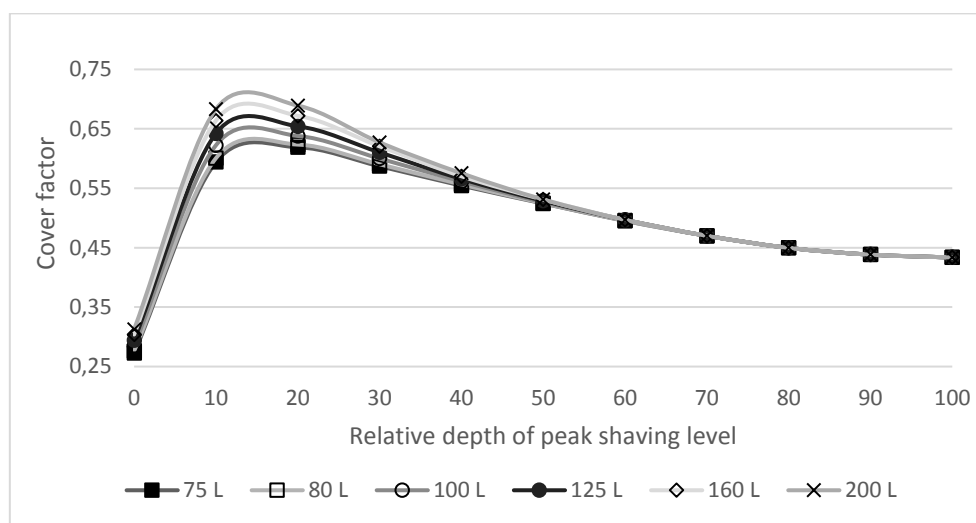


Figure 3. Cover factor at different generation graph shaving levels at different preheating boiler capacities

As mentioned in the previous section, maximal cover factor values are not applicable, as they cause additional losses in form of excess energy diverted into drain.

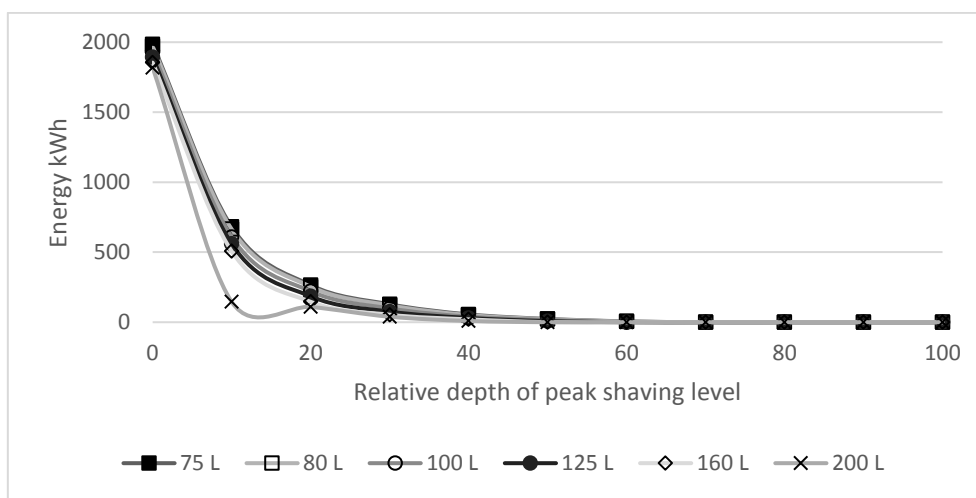


Figure 4. Drain losses of the preheating boiler in dependence of shaving levels at different volumes

At drain losses limited to 10 % of the boiler's energy balance, i.e. 184 kWh/y, the cover factors are shown in Table 1. At double boiler volume, i.e. at 160 l, the cover factor becomes equal to 0.68.

Table 1. Cover factor values at preheating boiler drain losses limited to 184 kWh/y

Boiler volume, l	Boiler heat capacity, kWh	Cover factor	Shaving level of generation charts, %
75	5.05	0.6	25
80	5.4	0.6	25
100	6.75	0.63	22
125	8.44	0.65	20
160	10.8	0.68	18
200	13.5	0.68	10
240	16.2	0.7	-

Further upsizing is not advantageous, as the cover factor gain is negligible and therefore not cost effective. In the other hand, at greater boiler volumes, the possibility of overheating and drain losses becomes less. The solution of

different shaving levels for wind turbine and solar panel generation graphs is yet to be checked. The processes should be evaluated in windier locations as well.

CONCLUSION

The electricity-to-heat energy conversion and storage contribute to more self-consumption in a residential building. Apart from the input power shaving levels, the self-consumption, expressed by the cover factor, is influenced by the heat storage capacity, i.e. the boiler volume. The conversion of electricity to heat is in this case irreversible – the heat cannot be converted to electricity. The self-consumption could be increased by another 10 % if the system would use electrical storage, but the feasibility of electrical storage in residential buildings is questionable at the current state of technology. The currently described increasing of self-consumption in residential buildings does not save energy. The main effect comes from cost savings derived from decreased energy purchases from the electricity grid. Nearly zero energy buildings have to use technologies with high energy efficiency to achieve energy saving, but these aspects were not in the focus of this study. Modelling shows, that at an annual wind/solar energy mix of 70/30, doubling the preheating boiler volume from 80 to 160 litres adds extra 8 % to the cover factor. A further upsizing does not bring additional benefits in terms of cost effectiveness, as the cover factor becomes „saturated“, i.e. its increase slows down.

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